



Sweden

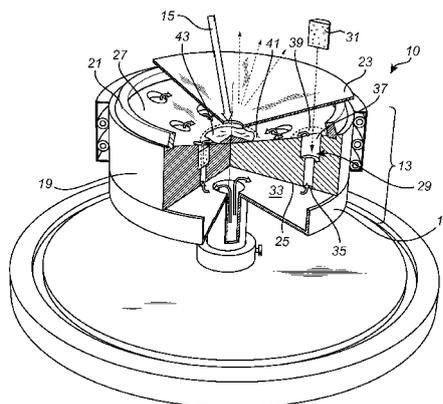
(12) Patent specification

(10) SE 539 684 C2

(21) Patent application number:	1651504-1	(51) Int.Cl.:	
(45) Grant of patent:	2017-10-31	<b>G21B 1/19</b>	(2006.01)
(41) Available to the public:	2017-10-31	G21B 3/00	(2006.01)
(22) Filing date:	2016-11-17		
(24) Effective date:	2016-11-17		
(30) Priority data:	---		

- (73) Patentee: Ultrafusion Nuclear Power UNP AB, Erik Dahlbergsgatan 11A, 411 26 Göteborg SE
- (72) Inventor: Leif Holmlid, MÖLNLYCKE SE
- (74) Agent: KRANSELL & WENNBORG KB, Box 2096, 403 12, Göteborg SE
- (54) Title: Apparatus for generating muons with intended use in a fusion reactor  
EP 2680271 A1 · XP 012199618 · US 20080008286 A1 · XP 029387484 · WO 2016093324 A1 · DE 102015114749 A1 · Holmlid L (2017) Mesons from Laser-Induced Processes in Ultra-Dense Hydrogen H(0). PLOS ONE 12(1): e0169895. <https://doi.org/10.1371/journal.pone.0169895>
- (56) Cited documents:
- (57) Abstract:

An apparatus (10) for generating muons, comprising: a hydrogen accumulator (13) including an inlet (35); an outlet (37) separated from the inlet by a flow path; a hydrogen transfer catalyst (31) arranged along the flow path between the inlet and the outlet; and an accumulating member (19) for receiving hydrogen in ultra-dense state from the outlet at a receiving portion (39) of the accumulating member and accumulating the hydrogen in the ultra-dense state at an accumulation portion (41) of the accumulating member. The accumulating member (19) has a downward sloping surface (27) from the receiving portion (39) to the accumulation portion (41). The apparatus further includes a field source (15), such as a laser, arranged to provide, to the accumulation portion (41) of the accumulating member (19), a field adapted to stimulate emission of negative muons from hydrogen in the ultra-dense state. The apparatus (10) further includes a specially designed barrier (21) and a shield (23) to retain the super-fluid ultra-dense hydrogen from creeping away from the accumulation portion of the generator.



ABSTRACT

An apparatus (10) for generating muons, comprising: a hydrogen accumulator (13) including an inlet (35); an outlet (37) separated from the inlet by a flow path; a hydrogen transfer catalyst (31) arranged along the flow path between the inlet and the outlet; and an accumulating member (19) for receiving hydrogen in ultra-dense state from the outlet at a receiving portion (39) of the accumulating member and accumulating the hydrogen in the ultra-dense state at an accumulation portion (41) of the accumulating member. The accumulating member (19) has a downward sloping surface (27) from the receiving portion (39) to the accumulation portion (41). The apparatus further includes a field source (15), such as a laser, arranged to provide, to the accumulation portion (41) of the accumulating member (19), a field adapted to stimulate emission of negative muons from hydrogen in the ultra-dense state.

15 The apparatus (10) further includes a specially designed barrier (21) and a shield (23) to retain the super-fluid ultra-dense hydrogen from creeping away from the accumulation portion of the generator.

## APPARATUS FOR GENERATING MUONS WITH INTENDED USE IN A FUSION REACTOR

### Field of the Invention

The present invention relates to an apparatus for generating muons.

### Background of the Invention

5 Fusion is one of the candidates for future large scale generation of energy without the emission problems associated with burning fossil fuel and the fuel disposal problem of traditional fission nuclear power.

Research into energy generation using fusion follows a number of parallel tracks. Most effort is currently spent on developing reactors for  
10 magnetic confinement fusion and inertial confinement fusion (ICF). Both of these tracks involve difficult problems, and it is unlikely that reliable and commercially viable fusion reactors using any of these techniques will be in operation in the near future.

An alternative process known as muon-catalyzed fusion has been  
15 known since the 1950's, and was initially seen as promising. However, it was soon realized that each muon, even if it were absolutely stable, could only catalytically react about 100 to 300 times because of a phenomenon known as "alpha-sticking" even in the most advantageous case of tritium-deuterium fusion. In addition, muons are unstable particles, which decay in about 2.2  $\mu$ s.

20 Existing methods of producing muons, for instance using proton accelerators, are expensive and much energy is required in the muon production. Hence, to make muon-catalyzed fusion practically useful, there is a need for a cheaper and more energy-efficient way of producing muons.

### 25 Summary

It is an object of the present invention to address the above, and to provide for energy generation by muon catalyzed fusion using ultra-dense hydrogen as the working substance for producing muons.

According to a first aspect of the present invention, it is therefore provided an apparatus for generating muons, comprising: a hydrogen accumulator including: an inlet for receiving hydrogen in a gaseous state; an outlet separated from the inlet by a flow path; a hydrogen transfer catalyst  
5 arranged along the flow path between the inlet and the outlet, the hydrogen transfer catalyst having a material composition being selected to cause a transition of hydrogen from the gaseous state to an ultra-dense state; and an accumulating member for receiving hydrogen in the ultra-dense state from the outlet at a receiving portion of the accumulating member and accumulating  
10 the hydrogen in the ultra-dense state at an accumulation portion of the accumulating member, the accumulating member being configured to provide a downward sloping surface from the receiving portion to the accumulation portion; and a field source arranged to provide, to the accumulation portion of the accumulating member, a field adapted to stimulate emission of negative  
15 muons from hydrogen in the ultra-dense state.

“Hydrogen” should, in the context of the present application, be understood to include any isotope or mix of isotopes where the nucleus has a single proton. In particular, hydrogen includes protium, deuterium, tritium and any combination of these.

20 By hydrogen in an “ultra-dense state” should, at least in the context of the present application, be understood hydrogen in the form of a quantum material (quantum fluid) in which adjacent nuclei are within much less than one Bohr radius of each other. In other words, the nucleus-nucleus distance in the ultra-dense state is considerably less than 50 pm. In the following,  
25 hydrogen in the ultra-dense state will be referred to as H(0) (or D(0) when deuterium is specifically referred to). The terms “hydrogen in an ultra-dense state” and “ultra-dense hydrogen” are used synonymously throughout this application.

A “hydrogen transfer catalyst” is any catalyst capable of absorbing  
30 hydrogen gas molecules ( $H_2$ ) and dissociating these molecules to atomic hydrogen, that is, catalyze the reaction  $H_2 \rightarrow 2H$ . The name hydrogen transfer catalyst implies that the so-formed hydrogen atoms on the catalyst

surface can rather easily attach to other molecules on the surface and thus be transferred from one molecule to another. The hydrogen transfer catalyst may further be configured to cause a transition of the hydrogen into the ultra-dense state if the hydrogen atoms are prevented from re-forming covalent  
5 bonds. The mechanisms behind the catalytic transition from the gaseous state to the ultra-dense state are quite well understood, and it has been experimentally shown that this transition can be achieved using various hydrogen transfer catalysts, including, for example, commercially available so-called styrene catalysts, as well as (purely) metallic catalysts, such as  
10 Iridium and Platinum. It should be noted that the hydrogen transfer catalyst does not necessarily have to transition the hydrogen in the gaseous state to the ultra-dense state directly upon contact with the hydrogen transfer catalyst. Instead, the hydrogen in the gaseous state may first be caused to transition to a dense state H(1), to later spontaneously transition to the ultra-dense state  
15 H(0). Also in this latter case, the hydrogen transfer catalyst has caused the hydrogen to transition from the gaseous state to the ultra-dense state.

In the dense state H(1), which is a higher-energy state than the ultra-dense state, the distance between adjacent nuclei is around 150 pm.

That ultra-dense hydrogen has actually been formed can be  
20 determined by irradiating the result of the catalytic reaction with a laser and then measuring the time of flight or velocity of the emitted particles. An example of such determination will be described in greater detail under the heading "Experimental results" further below.

The properties of ultra-dense hydrogen and methods for causing  
25 gaseous hydrogen to transition to ultra-dense hydrogen using different types of hydrogen transfer catalysts, as well as methods for detecting the presence and location of ultra-dense hydrogen, have been studied extensively by the present inventor and others. Results of these studies have, for example, been published in:

30 S. Badiiei, P.U. Andersson, and L. Holmlid, *Int. J. Hydrogen Energy* 34, 487 (2009);

S. Badiei, P.U. Andersson, and L. Holmlid, *Int. J. Mass. Spectrom.* 282, 70 (2009);

L. Holmlid, *Eur. Phys. J. A* 48 (2012) 11; and

P.U. Andersson, B. Lönn, and L. Holmlid, *Review of Scientific Instruments* 82, 013503 (2011).

Each of these scientific articles is hereby incorporated by reference in its entirety.

It should be understood that the above-mentioned downward sloping surface from the receiving portion to the accumulation portion of the accumulating member is downwards sloping when the apparatus for muon generation according to embodiments of the present invention is set up for operation.

The present invention is based on the realization that muons can be generated cheaper and more energy efficiently than using conventional methods, by accumulating ultra-dense hydrogen and subjecting the accumulated ultra-dense hydrogen to a perturbing field (such as an electromagnetic field, including purely electric or magnetic fields). The present inventor has further realized that ultra-dense hydrogen can be accumulated by providing a downward sloping surface between one or several supply locations for ultra-dense hydrogen and an accumulation portion. Through this configuration, gravity and feed gas flow will co-operate to move the ultra-dense hydrogen from the supply locations to the accumulation portion, where ultra-dense hydrogen is thus accumulated and can be subjected to the perturbing field, such as laser radiation, to generate muons.

According to embodiments of the apparatus according to the invention, the hydrogen accumulator may further comprise: a hydrogen flow barrier surrounding the receiving portion, the accumulation portion and the downward sloping surface for reducing escape of hydrogen in the ultra-dense state from the receiving portion away from the accumulation portion.

Due to the super-fluid properties of ultra-dense hydrogen, the ultra-dense hydrogen will flow upwards, away from the accumulating portion. The provision of the above-mentioned hydrogen flow barrier can prevent, or at

least substantially reduce the escape of ultra-dense hydrogen, which is due to the super-fluid properties of the ultra-dense hydrogen. Accordingly, the ratio of accumulated ultra-dense hydrogen to escaped ultra-dense hydrogen can be increased, which in turn provides for more efficient muon generation.

5           The barrier may advantageously have at least an outer surface facing the surrounded area that is made of a material that does not support creeping of ultra-dense hydrogen. Examples of such materials include various polymers, glass, and base metal oxides, such as aluminum oxide.

          According to various embodiments, the hydrogen accumulator may  
10 further comprise a shielding member arranged between the accumulating member and the field source and shielding the outlet and the receiving portion.

          The provision of a shielding member may further reduce escape of ultra-dense hydrogen, and may further protect the hydrogen transfer catalyst,  
15 at least in embodiments where the hydrogen transfer catalyst would otherwise be exposed to laser radiation.

          Furthermore, the shielding member may advantageously be arranged to expose the accumulation portion to the field provided by the field source. In embodiments where the above-mentioned perturbing field is provided in the  
20 form of laser radiation, the shielding member may be open over the accumulation portion to allow the laser radiation to hit the accumulated ultra-dense hydrogen in the accumulation portion.

          As described above for the barrier, at least a surface of the shielding member facing the accumulating member may be made of a material  
25 selected from the group consisting of a polymer, and a base metal oxide, to reduce creeping of ultra-dense hydrogen.

          According to various embodiments, furthermore, the hydrogen accumulator may further comprise a metallic absorbing member for absorbing hydrogen in the ultra-dense state, arranged in the accumulation portion of the  
30 hydrogen accumulating member.

Hereby, the super-fluid ultra-dense hydrogen can be retained in the accumulation portion, which provides for a more efficient generation of muons.

Advantageously, the metallic absorbing member may be made of at least one material selected from the group consisting of a metal in a liquid state at an operating temperature for the apparatus, and a catalytically active metal in a solid state at the operating temperature for the apparatus.

Examples of suitable materials for the metallic absorbing member include liquid or easily melted metals like Ga or K, and solid catalytically active metals like Pt or Ni etc.

According to various embodiments, the apparatus of the invention may further comprise a heating arrangement for increasing a temperature of the accumulating member comprised in the hydrogen accumulator.

By increasing the temperature of the accumulating member, the ultra-dense hydrogen can be transitioned from a super fluid to a normal fluid, which may reduce the amount of ultra-dense hydrogen escaping from the accumulating member through super-fluid creeping.

According to embodiments, moreover, the outlet may be arranged at the receiving portion of the accumulating member. Further, the outlet may be an integral portion of the accumulating member.

The hydrogen transfer catalyst may advantageously be porous, so that the hydrogen in the gaseous state can flow through the pores. This will provide for a large contact area between the hydrogen gas and the hydrogen transfer catalyst. At the same time, however, flow through the pores only will limit the attainable flow rate and thus possibly the rate of production of ultra-dense hydrogen.

The present inventor has found that flow through the pores of the hydrogen transfer catalyst is not necessary for causing the transition of the hydrogen from the gaseous state to the ultra-dense state, but that the hydrogen transfer catalyst is capable of causing this transition at a larger distance and more efficiently than was previously believed. Accordingly, the

hydrogen gas can be allowed to flow over a surface of the hydrogen transfer catalyst rather than be forced to flow through the hydrogen transfer catalyst.

According to various aspects, furthermore, the field source may be a laser arranged to irradiate hydrogen in the ultra-dense state accumulated in  
5 the accumulation portion of the accumulating member; the accumulating member comprised in the hydrogen accumulator may have an lower face and a concave upper face with a plurality of holes extending from the lower face to the concave upper face, each hole in the plurality of holes defining a flow path having an inlet on the lower face and an outlet on the upper face, a lowest  
10 portion of the upper concave face being the accumulation portion; and each of the holes may accommodate a hydrogen transfer catalyst having the material composition being selected to cause transition of hydrogen from the gaseous state to the ultra-dense state. Further, a barrier may surround the upper face; and a shielding member having a shielding member opening is  
15 arranged to, together with the barrier and the upper face form a partly enclosed space for preventing escape of hydrogen in the ultra-dense state, while allowing the laser to irradiate the accumulation portion through the shielding member opening.

Moreover, the apparatus for generating muons, according to various  
20 embodiments of the present invention may advantageously be included in a fusion reactor, further comprising a hydrogen vessel, wherein the apparatus is arranged to generate negative muons impinging on the hydrogen vessel, to catalyze fusion in the hydrogen vessel.

In summary, the present invention relates to an apparatus for  
25 generating muons, comprising: a hydrogen accumulator including an inlet; an outlet separated from the inlet by a flow path; a hydrogen transfer catalyst arranged along the flow path between the inlet and the outlet; and an accumulating member for receiving hydrogen in ultra-dense state from the outlet at a receiving portion of the accumulating member and accumulating  
30 the hydrogen in the ultra-dense state at an accumulation portion of the accumulating member. The accumulating member has a downward sloping surface from the receiving portion to the accumulation portion. It has also

several advanced features for handling the superfluid ultra-dense material like a barrier and a shield. The apparatus further includes a field source, such as a laser, arranged to provide, to the accumulation portion of the accumulating member, a field adapted to stimulate emission of negative muons from  
 5 hydrogen in the ultra-dense state.

#### Brief Description of the Drawings

These and other aspects of the present invention will now be described in more detail, with reference to the appended drawings showing example  
 10 embodiments of the invention, wherein:

Fig 1 is a schematic block diagram of a fusion reactor including a muon generator according to embodiments of the present invention;

Fig 2 is an exploded perspective view of an example embodiment of the apparatus for generating muons, according to the present invention;

15 Fig 3 is a schematic illustration of an exemplary measurement setup for detecting generation of negative muons;

Fig 4 is a diagram of measurements obtained using a similar setup as that shown in fig 3.

#### 20 Detailed Description of Example Embodiments

Fig 1 is a schematic block diagram functionally illustrating a fusion reactor for muon catalyzed fusion using muon generator according to embodiments of the present invention.

25 The fusion reactor 1 comprises a muon generator 10, a vessel 3 containing hydrogen gas (which may, for example, be a suitable mix of protium, deuterium, and tritium), a vaporizer 5, and an electrical generator 7.

As is schematically shown in fig 1, muons generated by the muon generator 10 are used for catalyzing fusion according to, *per se*, known fusion reactions in the vessel 3. Heat resulting from the fusion reactions in the  
 30 vessel 3 is used for vaporizing a process fluid, such as water, in the vaporizer. The resulting vapor-phase process fluid, such as steam, is used to

drive the electrical generator 7, resulting in output of electrical energy. If only heat is needed, the electrical generator is not needed.

Fig 2 is a schematic illustration of an example embodiment of the apparatus for generating muons according to the present invention. In the following, the apparatus will generally be referred to as “muon generator”.

With reference to fig 2, the muon generator 10 comprises a hydrogen accumulator 13, and a field source, here in the form of a laser (not shown in fig 2, but represented by a block arrow illustrating a laser beam 15). As is schematically indicated in fig 2, the hydrogen accumulator 13 comprises a hydrogen gas intake member 17, an accumulating member 19, a barrier 21, here in the form of a gasket and a shielding member 23.

As is shown in fig 2, the accumulating member 19 has a lower face 25 and a concave upper face 27. In the particular example shown in fig 2, the concave upper face 27 is generally conical, with a rounded apex. A plurality of holes 29 (only one of the holes is indicated by a reference numeral to avoid cluttering the drawings) extend through the accumulating member 19 from the lower face 25 to the upper face 27, and a corresponding plurality of hydrogen transfer catalyst plugs 31 (only one of the catalyst plugs is indicated by a reference numeral to avoid cluttering the drawings) are accommodated by the holes 29.

In the example embodiment of fig 2, the lower face 25 of the accumulating member 19 forms the lid of an inlet chamber 33 for hydrogen gas, further defined by the hydrogen gas intake member 17. Each of the holes 29 formed through the accumulating member 19 has an inlet 35 for receiving hydrogen gas from the inlet chamber 23, and an outlet 37 for providing ultra-dense hydrogen to receiving portions 39 on the upper face 27 of the accumulating member 19.

Due to the conical shape of the upper face 27 of the accumulating member 19, the ultra-dense hydrogen provided to the receiving portions 39 tends to mainly flow towards the accumulation portion 41 at the bottom of the “bowl” formed by the upper face 27 of the accumulating member 19.

Due to the super-fluid behavior of ultra-dense hydrogen (below a transition temperature between the super-fluid state and the normal-fluid state of ultra-dense hydrogen), some of the ultra-dense hydrogen provided to the receiving portions 39 may flow upwards, away from the accumulation portion  
5 41. This flow is hindered by the barrier 21, and also by the shielding member 23.

To even further increase the amount of ultra-dense hydrogen in the accumulation portion 41, the hydrogen accumulating member 13 additionally comprises an ultra-dense hydrogen retaining member 43 arranged in the  
10 accumulation portion 41. The ultra-dense hydrogen retaining member 43 may, as was explained further above in the Summary section, be made of a liquid metal or a solid metal capable of absorbing ultra-dense hydrogen.

It should be noted that many different shapes of the concave upper face 27 are possible. For instance, the concave upper face 27 need not be  
15 rotationally symmetrical, as long as there is a sloping surface portion from the receiving portion(s) 29 towards the accumulation portion 41.

The ultra-dense hydrogen accumulated in the accumulation portion 41 is subjected to a perturbing field using the field source (indicated by the laser beam 15). In the example embodiment of fig 2, the field source is a laser and  
20 the perturbing field is thus provided in the form of laser radiation.

The person skilled in the art realizes that the present invention by no means is limited to the preferred embodiments described above. On the contrary, many modifications and variations are possible within the scope of the appended claims.

25 In the claims, the word "comprising" does not exclude other elements or steps, and the indefinite article "a" or "an" does not exclude a plurality. The mere fact that certain measures are recited in mutually different dependent claims does not indicate that a combination of these measured cannot be used to advantage.

30

#### Theoretical discussion

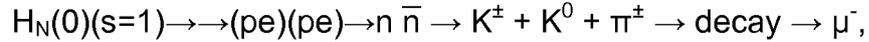
#### *Ultra-dense hydrogen and muon generation*

Ultra-dense hydrogen H(0) is a quantum material at room temperature. It is described in several scientific publications, with detailed studies of the structure of D(0) and also of its protium analog p(0). It is shown to be both superfluid and superconductive at room temperature. Due to the normally  
 5 measured very short p-p and D-D distances of 2.3 pm and below, the density of H(0) is very high.

While ordinary (orbital angular momentum  $l$ ) based Rydberg matter has  $l > 0$  for its binding electrons, this ultra-dense matter has  $l = 0$  and  $s > 0$  (1, 2, 3, 4...) which is the spin quantum number for the binding electrons. Thus, the  
 10 electrons which give the ultra-dense matter structure have no orbital motion, but only a spin motion. This electron spin motion may be interpreted as a motion of the charge with orbit radius  $r_q = \hbar/2m_e c = 0.192$  pm and with the velocity of light  $c$  ('Zitterbewegung'). This spin motion is centered on the H atoms and may give a planar structure for the H-H pairs as in the case of the  
 15 planar clusters for ordinary Rydberg matter. This means that the interatomic distance in ordinary Rydberg matter which is  $d = 2.9 l^2 a_0$  is replaced with  $d = 2.9 s^2 r_q$  for the ultra-dense matter, as verified by direct measurements. Here, 2.9 is a constant determined numerically for ordinary Rydberg matter and confirmed experimentally by radio frequency spectroscopy. It is also  
 20 confirmed for ultra-dense hydrogen by visible emission spectroscopy. The Bohr radius is indicated as  $a_0$ . The spin-circling electronic charges provide the necessary shielding of the nuclei which keeps the material strongly bound, similar to ordinary Rydberg matter but with much larger binding energies.

The mechanism of formation of ultra-dense matter starts with the  
 25 formation of higher normal Rydberg matter levels ( $l = 1-3$ ), which are formed spontaneously at the catalyst surface. It implies that the ultra-dense hydrogen is formed from ordinary Rydberg matter levels  $l = 1-3$  falling down to the lower energy ultra-dense states. The nuclear processes taking place in H(0) spontaneously and under laser impact or other field induction processes are  
 30 still not completely known. However, several different steps have been studied separately. For example, the laser induces the transition from  $s=2$  to  $s=1$  in H(0). The total process giving the negative muons required for the

muon-catalyzed fusion starts with the ultra-dense hydrogen particles  $H_N(0)$  and is proposed to be:



5

where  $\bar{n}$  is an anti-neutron, formed from the "quasi-neutrons" (pe) (proton + electron). The mesons formed are all types of kaons and pions, and it is likely that three kaons are formed from each  $H_N(0)$  particle since this conserves the number of quarks. Over all, the number of quarks is largely unchanged in the meson formation step, but further pair production of pions is also possible which does not conserve the number of quarks. The process shown is highly exoergic and gives much more than 100 MeV to the particles ejected from each pair of protons. This should be compared to ordinary D+D fusion, which has an output per pair of deuterons of 4-14 MeV depending on the conditions like temperature.

15

#### *Catalytic conversion*

The catalytic process for converting hydrogen gas to ultra-dense hydrogen may employ commercial so called styrene catalysts, i.e. a type of solid catalyst used in the chemical industry for producing styrene (for plastic production) from ethylene benzene. This type of catalyst is made from porous Fe-O material with several different additives, especially potassium (K) as so called promoter. The function of this catalyst has been studied in detail by several different groups.

The catalyst is designed to split off hydrogen atoms from ethyl benzene so that a carbon-carbon double bond is formed, and then to combine the hydrogen atoms so released to hydrogen molecules which easily desorb thermally from the catalyst surface. This reaction is reversible: if hydrogen molecules are added to the catalyst they are dissociated to hydrogen atoms which are adsorbed on the surface. This is a general process in hydrogen transfer catalysts. We utilize this mechanism to produce ultra-dense

30

hydrogen, which requires that covalent bonds in hydrogen molecules are not allowed to form after the adsorption of hydrogen in the catalyst.

The potassium promoter in the catalyst provides for a more efficient formation of ultra-dense hydrogen. Potassium (and for example other alkali  
5 metals) easily forms so called circular Rydberg atoms  $K^*$ . In such atoms, the valence electron is in a nearly circular orbit around the ion core, in an orbit very similar to a Bohr orbit. At a few hundred °C not only Rydberg states are formed at the surface, but also small clusters of Rydberg states  $K_N^*$ , in a form called Rydberg Matter (RM).

10 The clusters  $K_N^*$  transfer part of their excitation energy to the hydrogen atoms at the catalyst surface. This process takes place during thermal collisions in the surface phase. This gives formation of clusters  $H_N^*$  (where H indicates proton, deuteron, or triton) in the ordinary process also giving the  $K_N^*$  formation, namely cluster assembly during the desorption process. If the  
15 hydrogen atoms could form covalent bonds, molecules  $H_2$  would instead leave the catalyst surface and no ultra-dense material could be formed. In the RM material, the electrons are not in so-called s orbitals since they always have an orbital angular momentum greater than zero. This implies that covalent bonds cannot be formed since the electrons on the atoms must be in  
20 s orbitals to form the normal covalent sigma ( $\sigma$ ) bonds in  $H_2$ . The lowest energy level for hydrogen in the form of RM is metallic (dense) hydrogen called H(1), with a bond length of 150 picometer (pm). The hydrogen material falls down to this level by emission of mainly infrared radiation. Dense hydrogen is then spontaneously converted to ultra-dense hydrogen called  
25 H(0) with a bond distance of 0.5 - 5 pm depending on the spin level. This material is a quantum material (quantum fluid) which may involve both electron pairs (Cooper pairs) and nuclear pairs (proton, deuteron or triton pairs, or mixed pairs). These materials are both superfluid and  
superconductive at room temperature, as confirmed in several experiments.

30

### Experimental results

Results are here given which characterize a muon generator like the apparatus 10 schematically shown in fig 2, with reference to fig 3 illustrating an experimental setup, and fig 4 showing results of measurements carried out  
5 using a similar experimental setup.

Referring to fig 3, the experimental setup comprises a vacuum chamber 51, the muon generator 10 described above with reference to fig 2, a toroidal coil 53, and a collector 55. There is a first distance  $d_1$  between the accumulation portion 41 and the coil, and a second distance  $d_2$  between the  
10 accumulation portion 41 and the collector 55. As is schematically indicated in fig 3, the vacuum chamber 51 has a window 54 for allowing passage of a laser beam 15. A lens 56 is provided inside the vacuum chamber 51 for focusing the laser beam 15 at the accumulation portion 41 of the muon generator 10.

15 The  $D_2$  gas pressure in the vacuum chamber 51 is around 1 mbar with constant pumping.

In the present experimental setup, the field source comprised in the muon generator is a pulsed laser with pulse length in the few nanosecond range. Both visible and infrared laser light give similar behavior. The pulse  
20 energy used for the typical experiments is of the order of 200 - 400 mJ. With a pulse repetition rate of 10 Hz typical, this means only 2 - 4 W of laser power outside the vacuum chamber. The effective laser power at the muon generator is somewhat lower, due to losses by reflection in beam steering mirrors, in the glass window 54 in the vacuum chamber wall and in the  
25 focusing lens 56.

The laser beam is normally focused on the accumulation portion 41 of the muon generator using a lens 56 of 40-50 mm focal length, but the focusing is not critical.

Experiments have been performed with a current transformer which  
30 directly measures the current from the laser-induced nuclear processes using the toroidal coil 53. A wire is there wound around a ferrite toroidal core, with around 20 turns of wire on a toroid of a few cm diameter. The pulse of

charges from the laser-induced nuclear processes on the generator is observed as an induced current in the coil. This is a standard method of measuring the pulse current for example in electron accelerators with the particles moving at relativistic velocities. In the present experiments, the  
 5 beam passing through the coil is additionally observed the foil collector 55. This means that absolute calibration is possible.

For a somewhat simplified measurement case using similar equipment as that schematically illustrated in fig 3, fig 4 shows a first signal 57 obtained from a coil, such as the coil 53 in fig 3, and a second signal 59 obtained from  
 10 a collector, such as the collector in fig 3. The known distance between the coil 53 and the collector 55 of about 1 m, and the measured delay of about 3 ns indicates charged particles traveling close to the speed of light. Since the coil only gives a signal due to charged particles, photons are excluded as the particles giving the signals.

15 The curve shape of the signal in Fig 4 agrees well with that calculated for a meson in a decay chain, with a time constant for the decay of 12 ns. This is the characteristic decay time for charged kaons  $K^\pm$ . In several published studies also characteristic decay times of 26 and 52 ns have been measured, indicating decay of charged pions  $\pi^\pm$  and neutral long-lived kaons  
 20  $K_L^0$ . It is well-known that all these particles decay to the much more long-lived muons  $\mu^\pm$ , which are the particles mainly observed in the coil and at the collector in Fig 4. Relevant publications include:

L. Holmlid, Int. J. Modern Phys. E 24 (2015) 1550026.

L. Holmlid, Int. J. Modern Phys. E 24 (2015) 1550080.

25 L. Holmlid, Int. J. Modern Phys. E 25 (2016) 1650085.

To ascertain that muons are formed, also several published studies have directly measured the decay of the muons and their interaction with matter including electron-positron pair production. The direct decay time of free muons at 2.2  $\mu$ s has also been measured, and slightly shorter decay  
 30 times due to muon interaction with other particles like nuclei. Relevant publications include:

L. Holmlid and S. Olafsson, *Int. J. Hydr. Energy* 40 (2015) 10559-10567.

L. Holmlid and S. Olafsson, *Rev. Sci. Instrum.* 86, 083306 (2015).

L. Holmlid and S. Olafsson, *Int. J. Hydrogen Energy* 41 (2016) 1080-5 1088.

S. Olafsson and L. Holmlid, *Bull. Am. Phys. Soc.* 2016/4/16.  
BAPS.2016.APR.E9.9.

CLAIMS

1. An apparatus (10) for generating muons, comprising:  
an ultra-dense hydrogen accumulator (13) including:  
5            an inlet (35) for receiving hydrogen in a gaseous state;  
              an outlet (37) separated from said inlet by a flow path;  
              a hydrogen transfer catalyst (31) arranged along the flow path  
between said inlet and said outlet, said hydrogen transfer catalyst having a  
material composition being selected to cause a transition of hydrogen from  
10 the gaseous state to an ultra-dense state; and  
              an accumulating member (19) for receiving hydrogen in the  
ultra-dense state from said outlet at a receiving portion (39) of the  
accumulating member and accumulating said hydrogen in the ultra-dense  
state at an accumulation portion (41) of the accumulating member, the  
15 accumulating member (19) being configured to provide a downward sloping  
surface (27) from said receiving portion (39) to said accumulation portion (41);  
and  
              a field source (15) arranged to provide, to the accumulation portion  
(41) of said accumulating member (19), a field adapted to stimulate or induce  
20 emission of negative muons from hydrogen in the ultra-dense state.
  
2. The apparatus (10) according to claim 1, wherein said hydrogen  
accumulator (13) further comprises:  
              a barrier (21) surrounding said receiving portion (39), said  
25 accumulation portion (41) and said downward sloping surface (27) for  
reducing escape of hydrogen in the ultra-dense state.
  
3. The apparatus (10) according to claim 2, wherein said barrier (21)  
has at least an outer surface made of a material selected from the group  
30 consisting of a polymer, and a base metal oxide.

4. The apparatus (10) according to any one of the preceding claims, wherein said hydrogen accumulator (13) further comprises:

5 a shielding member (23) arranged between said accumulating member (19) and said field source (15) and shielding said outlet (37) and said receiving portion (39).

5. The apparatus (10) according to claim 4, wherein said shielding member (23) is arranged to expose said accumulation portion (41) to the field provided by said field source (15).

10

6. The apparatus (10) according to claim 4 or 5, wherein at least a surface of said shielding member (23) facing said accumulating member (19) is made of a material selected from the group consisting of a polymer, a base metal oxide, and a metal.

15

7. The apparatus (10) according to any one of the preceding claims, wherein said hydrogen accumulator (13) further comprises:

20 a metallic absorbing member (43) for absorbing hydrogen in the ultra-dense state, arranged in said accumulation portion (41) of the hydrogen accumulating member (19).

8. The apparatus (10) according to claim 7, wherein said metallic absorbing member (43) is made of at least one material selected from the group consisting of a metal in a liquid state at an operating temperature for said apparatus and a catalytically active metal in a solid state at the operating temperature for said apparatus.

9. The apparatus (10) according to any one of the preceding claims, further comprising a heating arrangement for increasing a temperature of the accumulating member (19) comprised in said hydrogen accumulator (13).

30

10. The apparatus (10) according to any one of the preceding claims, wherein said outlet (37) is arranged at the receiving portion (39) of said accumulating member (19).

5           11. The apparatus (10) according to claim 10, wherein said outlet (37) is an integral portion of said accumulating member (19).

12. The apparatus (10) according to any one of the preceding claims, wherein said field source (15) is a laser arranged to irradiate the accumulation  
10 portion (41) of said accumulating member (19) of the hydrogen accumulator (13).

13. The apparatus (10) according to claim 1,  
          wherein said field source is a laser (15) arranged to irradiate hydrogen  
15 in the ultra-dense state accumulated in the accumulation portion (41) of said accumulating member (19);

          wherein the accumulating member (19) comprised in said hydrogen accumulator (13) has an lower face (25) and a concave upper face (27) with a plurality of holes (29) extending from said lower face to said concave upper  
20 face, each hole in said plurality of holes defining a flow path having an inlet (35) on said lower face and an outlet (37) on said upper face, a lowest portion of said upper concave face being said accumulation portion (41);

          wherein each of said holes (29) accommodates a hydrogen transfer catalyst (31) having said material composition being selected to cause  
25 transition of hydrogen from the gaseous state to the ultra-dense state;

          wherein a barrier (21) surrounds said upper face (27); and

          wherein a shielding member (23) having a shielding member opening is arranged to, together with said barrier (21) and said upper face (27) form a partly enclosed space for preventing escape of hydrogen in the ultra-dense  
30 state, while allowing said laser (15) to irradiate said accumulation portion (41) through said shielding member opening.

14. A fusion reactor (1) comprising:  
a hydrogen vessel (3); and  
an apparatus (10) according to any one of the preceding claims,  
arranged to generate negative muons impinging on said hydrogen vessel, to  
5 catalyze fusion in said hydrogen vessel.

I följande bilaga finns en översättning av patentkraven till svenska. Observera att det är patentkravens lydelse på engelska som gäller.

A Swedish translation of the patent claims is enclosed. Please note that only the English claims have legal effect.

KRAV

1. Anordning (10) för generering av muoner, innefattande:  
en ultralätt väteackumulator (13) innefattande:

- 5 ett inlopp (35) för mottagande av väte i ett gasformigt tillstånd;  
ett utlopp (37) separerat från nämnda inlopp genom en  
flödesbana;  
en väteöverföringskatalysator (31) anordnad längs flödesbanan  
mellan nämnda inlopp och nämnda utlopp, nämnda väteöverförings-  
10 katalysator med en materialkomposition vald för att orsaka en övergång av  
väte från gasformigt tillstånd till ett ultra-tätt tillstånd; och  
ett ackumulerande element (19) för mottagande av väte i det  
ultra-täta tillståndet från nämnda utlopp vid en upptagande del (39) hos  
ackumuleringsdelen och ackumulering av nämnda väte i det ultra-täta  
15 tillståndet vid en ackumuleringsdel (41) hos ackumuleringsdelen , varvid det  
ackumulerande elementet (19) är konfigurerat att åstadkomma en  
nedåtgående sluttande yta (27) från nämnda mottagningsdel (39) till  
ackumuleringsdelen (41); och  
en fältkälla (15) anordnad att till ackumuleringsdelen (41) av  
20 ackumuleringsdelen (19) tillhandahålla ett fält anpassat för att stimulera eller  
inducera utsläpp av negativa muoner från väte i det ultra-täta tillståndet.

2. Anordning (10) enligt krav 1, varvid väteackumulatorm (13) vidare  
innefattar:

- 25 en barriär (21) som omger nämnda mottagande del (39),  
ackumuleringsdelen (41) och den nedåtgående sluttande ytan (27) för att  
reducera utsläpp av väte i det ultra-täta tillståndet.

3. Anordning (10) enligt krav 2, varvid nämnda barriär (21) har  
30 åtminstone en yttre yta gjord av ett material valt från gruppen bestående av  
en polymer och en basmetalloxid.

4. Anordning (10) enligt något av föregående patentkrav, varvid väteackumulatorn (13) vidare innefattar:

5 en skärmdel (23) anordnad mellan ackumuleringselementet (19) och fältkällan (15) och avskärmning av nämnda utlopp (37) och mottagardelen (39).

5. Anordning (10) enligt krav 4, varvid nämnda skärmdel (23) är anordnad att exponera ackumuleringsdelen (41) till fältet som tillhandahålls av nämnda fältkälla (15).

10

6. Anordning (10) enligt krav 4 eller 5, varvid åtminstone en yta av skärmdelen (23) vänd mot ackumuleringsdelen (19) är tillverkad av ett material valt från gruppen bestående av en polymer, en basmetalloxid och en metall.

15

7. Anordning (10) enligt något av föregående krav, varvid väteackumulatorn (13) vidare innefattar:

20 ett metallabsorberande element (43) för absorption av väte i det ultratäta tillståndet, anordnat i ackumuleringsdelen (41) hos väteackumuleringsdelen (19).

8. Anordning (10) enligt krav 7, varvid det metallabsorberande elementet (43) är tillverkat av åtminstone ett material valt från gruppen bestående av en metall i flytande tillstånd vid en driftstemperatur för apparaten och en katalytiskt aktiv metall i ett fast tillstånd vid driftstemperaturen för nämnda apparat.

9. Anordning (10) enligt något av föregående patentkrav, vidare innefattande ett uppvärmningsarrangemang för att öka en temperatur hos ackumuleringsdelen (19) som ingår i väteackumulatorn (13).

30

10. Anordning (10) enligt något av föregående krav, varvid utloppet (37) är anordnat vid det ackumulerande elementets (19) mottagardel (39).

11. Anordning (10) enligt krav 10, varvid utloppet (37) är en integrerad  
5 del av ackumuleringsdelen (19).

12. Anordning (10) enligt något av föregående krav, varvid nämnda fältkälla (15) är en laser anordnad att bestråla ackumuleringsdelen (41) hos ackumuleringsdelen (19) hos väteackumulatorn (13).

10

13. Anordning (10) enligt krav 1,

varvid nämnda fältkälla är en laser (15) anordnad att bestråla väte i det ultra-täta tillståndet ackumulerat i ackumuleringsdelen (41) hos nämnda ackumuleringsdel (19);

15

varvid det ackumulerande elementet (19) som ingår i väteackumulatorn (13) har en nedre yta (25) och en konkav övre yta (27) med ett flertal hål (29) som sträcker sig från nämnda undre yta till den konkava övre ytan, varvid varje hål i nämnda flertal hål som definierar en flödesbana som har ett inlopp (35) på nämnda undre yta och ett utlopp (37) på nämnda övre yta, varvid en  
20 lägsta del av den övre konkava ytan är nämnda ackumuleringsdel (41);

varvid var och en av nämnda hål (29) upptar en väteöverföringskatalysator (31) med vilken materialkompositionen väljs för att orsaka övergång av väte från gasformigt tillstånd till det ultra-täta tillståndet;

varvid en barriär (21) omger nämnda övre yta (27); och

25

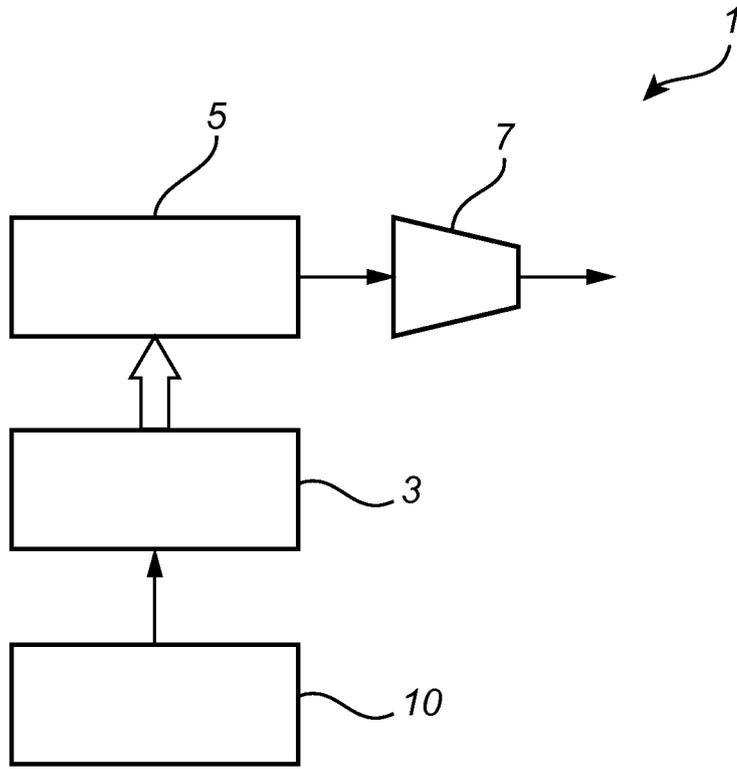
varvid en avskärmningsdel (23) som har en skärmningsöppning är anordnad att tillsammans med barriären (21) och nämnda övre yta (27) bilda ett delvis inneslutet utrymme för att förhindra att väte avlägsnas i det ultra-täta tillståndet medan man tillåter nämnda laser (15) för att bestråla nämnda ackumuleringsdel (41) genom nämnda avskärmningsorganöppning.

30

14. En fusionsreaktor (1) innefattande:

ett vätekärl (3); och

en anordning (10) enligt något av föregående krav, anordnad att alstra negativa muoner som påverkar nämnda vätekärl för att katalysera fusion i vätekärlet.



*Fig. 1*

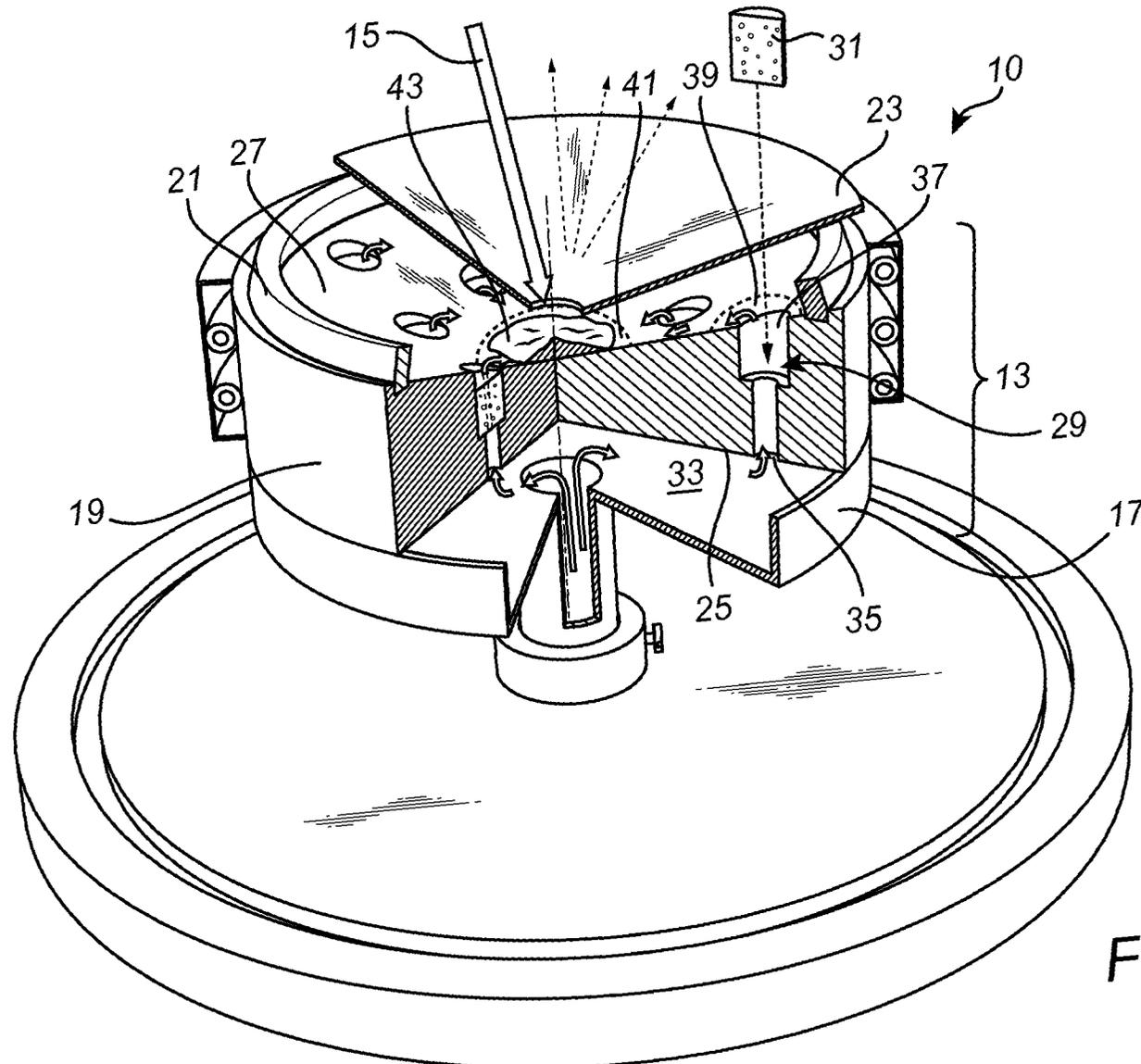


Fig. 2

3/4

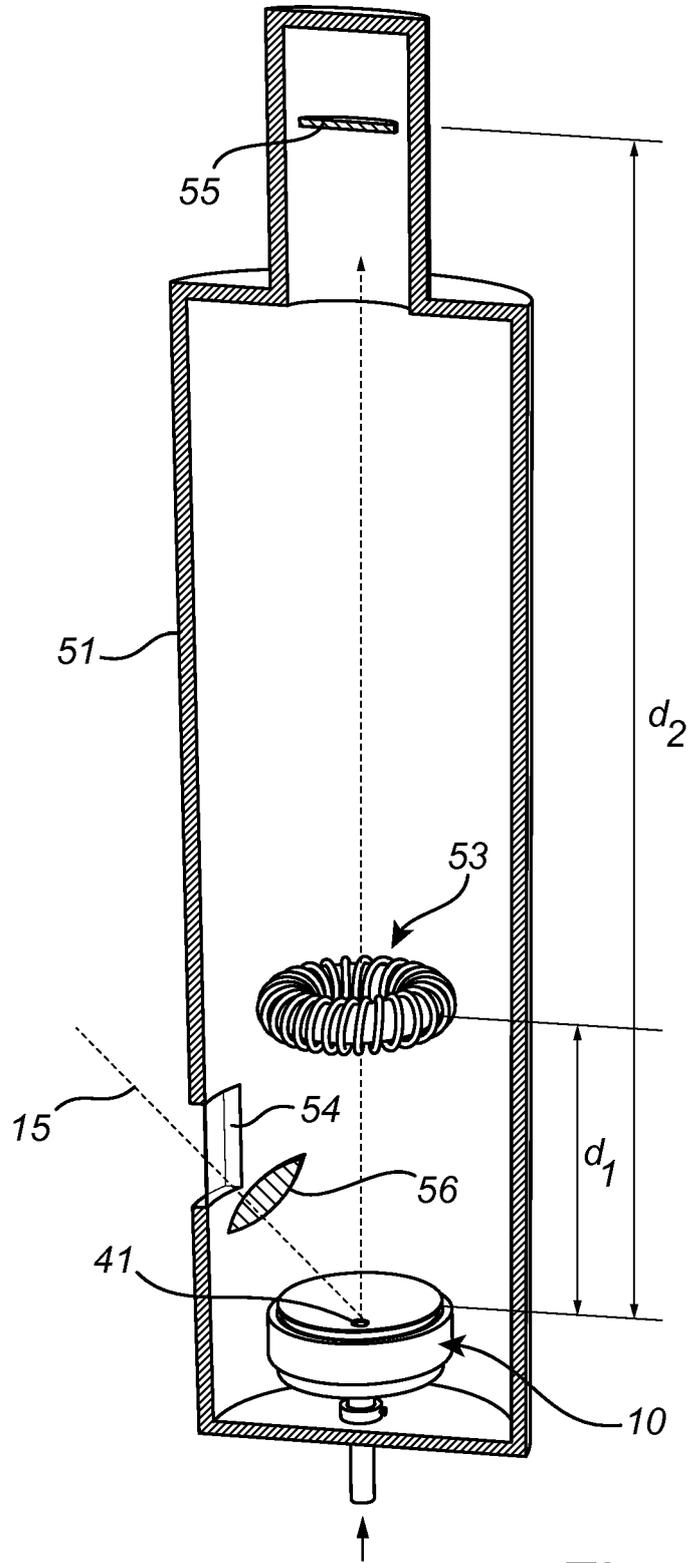
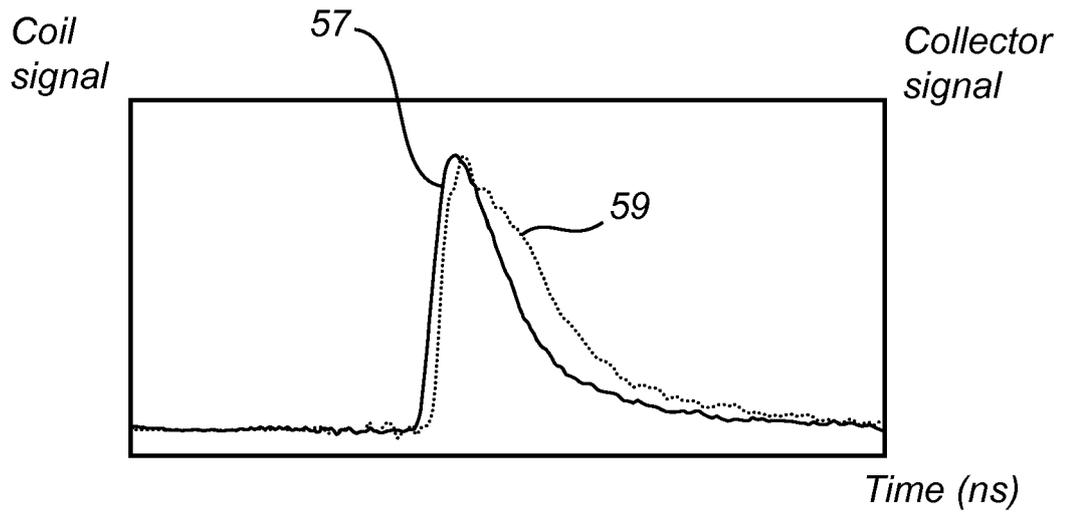


Fig. 3



*Fig. 4*